







DESIGN CONCEPT FOR FUEL FIRE FACILITY SCALE-DOWN

John R. Piergallini
Aircraft and Crew Systems Technology Directorate
NAVAL AIR DEVELOPMENT CENTER
Warminster, Pennsylvania 18974

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UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER 4D-A084 6a NADC-79227-60 TITLE (and Subtitle) TYPE OF REPORT & PERIOD COVERED Design Concept For Fuel Fire FINAL REPORTIN Facility Scale-Down AUTHOR(a) B. CONTRACT OR GRANT NUMBER(e) /Piergallini John R. PERFORMING ORGANIZATION NAME AND ADDRESS PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Aircraft and Crew Systems Technology Directorate Airtask WF51-523-000 Naval Air Development Center P.E. 62758N Warmir ster PA 18974 11. CONTEJLLING OFFICE NAME AND ADDRESS 12, REPORT DATE Naval Air Systems Command 20 AUGHT Department of the Navy Washington DC 20361
MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office) 5. SECURITY CLASS. (of this report) UNCLASSIFIED 184. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) Arproved for Public Release; Distribution unlimited. 18. STAPLEMENTARY NOTES 19 KEY WORDS (Continue on reverse side if necessary and identify by block number) Fuel Fire Test Facility Thermal Hazard of Fire Contact Personal Protection From Flame Contact of the itady 20. ARST RACT (Continue on reverse side if necessary and identify by block number) The objective is to provide an all-weather, self-sustaining, indoor fuel-fire facility for the generation of data for the evaluation of burn-protective capacity of personal gear for naval aircrewmen and flight deck personnel in full-scale fuel fire exposures. A scaled-down indoor version of the existing fuel-fire facility will provide realistic data for protective-capacity analysis. Construction of an automated enclosed facility will allow experiments to be conducted efficiently indoors in a closely controlled environment with minimal risk to personnel and surroundings and with more timely and consis DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

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OBJECTIVE

A full-scale fuel fire facility with associated equipment and instrumentation exists for the purpose of predicting the protective capacity of personal gear of naval aircrewmen and flight deck personnel exposed to the thermal hazard of fuel fires in aircraft crashes such as may occur on a carrier deck (reference 1). It is the aim of this investigation to conduct a feasibility study for construction of a scaled-down version of the fuel facility so that experiments can be conducted efficiently indoors in a closely controlled environment with minimal risk to personnel and surroundings.

PROCEDURE

With the existing facility, a full-scale fuel fire test normally employs seven skilled personnel. Four operate the pit and instrumentation and three document the procedures in motion picture and still photographic coverage. In addition to these personnel, specific limitations are imposed by the wind velocity, direction of the wind, precipitation conditions, ambient temperature, etc. A scaled-down indoor facility will permit all-weather operation, reduce the number of personnel required for operational testing and improve logistics by limiting the transporting of manikins, clothing, instrumentation, fuel, water and photographic, operational and fire department personnel. An indoor facility will also improve maintainability and reliability and increase productivity by reducing the number of test exposures needed for valid assessments of protectivity and the costs of material assembly.

RESULTS AND DISCUSSION

In the design of a new fuel fire facility, the foremost considerations must include reduction in size, containment, and automation. In the present plans, utilization of existing proven designs with improvements are incorporated in the fuel ignition system, fuel dispersion and grating system, power, timing and control circuitry, data collection and recording system, and the fuel and water pit holding system. New design considerations for the scaled-down version include protective and retaining walls, a ventilation and exhaust system, a traversing system and a fire extinguishing system. To this end the following plans with identification drawing numbers have been developed for consideration and incorporation in the design of the new facility and are shown in this report as appendix A, B, C, and D.

NAVFAC DRAWING NUMBER

2002346	Install	Fuel	Distribution	And	Ignition	System
2002347	Install	Fuel	Distribution	And	Ignition	System
2002348	Install	Fuel	Distribution	And	Ignition	System

ENGINEERING RESOURCES INC. DRAWING NUMBER

D	00041	Fuel Ignition System
D	00042	Fuel Ignition System
D	00044	Fuel Dispersion System
SKC	00043	Piping And Nozzle Details
J	00041	Fuel Pumping System

W. N. BEST COMBUSTION EQUIPMENT CO., INC. DRAWING NUMBER

11273	Orifice Assembly Ignitor Gas Line
22524	Piping Schematic
22525-1	Fuel Ignition System - Ignitor, Heat Shield And Mounting Arrangement
30162	Fuel Gas Ignitor Wiring
11124	Ignitor

ENVIRONMENTAL PHYSIOLOGY DRAWING NUMBER

υ01	Fuel	Fire	Facility	Scale	Down
002	Fuel	Fire	Facility	Scale	Down
003	Fue1	Fire	Facility	Scale	Down

The design concept for each phase of development of the scaled-down version of the fuel fire facility follows:

Fuel Dispersion and Grating System - Aside from the architectural design of the fuel dispersion and grating system which is diagrammed in Environmental Physiology Drawing No. 1, 2, and 3 of appendix D. This system must be improved to prevent existing problems which occur because of corrosion and expansion. The fuel dispersion system is currently constructed of galvanized steel which is continually immersed in water causing the orifice assemblies to become contaminated with rust preventing and even distribution of fuel in each containment cell. It is therefore recommended that stainless steel or copper piping be used throughout to correct the problem. In addition, during a full scale fuel fire the grating system expands considerably and in some instances buckles because of the extreme heat and a lack of clearance at the ends. For a temperature differential of 650°C, aluminum elongates 4.7 inches for each 20 foot length. Stainless steel is recommended as a replacement for the aluminum because it has a lower coefficient of expansion and improved corrosive properties.

Ignition, Power, Timing and Control System - Currently the ignition, power, timing and control systems are functional but their proximity to the fuel fire creates a hazard to the operating personnel manning the three control stations

during exposures. An automated system with one control console at a remote site will improve test coordination and reduce risk to operational personnel.

Pit with Protective and Retaining Walls - The pit will be constructed of reinforced concrete with overall inside dimensions of 16 feet by 6 feet by 8 inches deep. The protective walls will be constructed of fire brick inside with a solid block exterior.

Ventilation and Exhaust System - The roof of the enclosed structure will be opened to the atmosphere during the fuel fire. Therefore, it will be constructed as a heavy gage steel louvered system operated electromechanically for ease of operation in opening and closing. Two 36 inch exhaust fans will provide sufficient air flow to adequately ventilate the fuel fire pit enclosure (1920 cubic feet) after each exposure.

Fire Extinguishing System - A carbon dioxide fire extinguisher system, for emergency use only, will be required in the event that the manikin is delayed in the fire because of a mechanical malfunction of the traversing system or in order to quickly abort an existing fire for some unforeseen reason.

Data Collection and Recording System - The telemetry data acquisition and display system, (reference 2) will be used for recording and analysis of data in the scaled-down version of the facility. The commutator, oscillator, transmitter, and antenna will be housed in the manikin. The antenna for the receiver will be located in the fuel fire pit area. The magnetic tape recorder, receiver, oscillograph, oscilloscope, and associated equipment will be located in the control room adjacent to the fuel fire pit. Provisions will be made for future development to include permanent heat flux sensors located throughout the pit enclosure so that at specified locations of the manikin in the fire, comparative measurements can be made of the temperature rise of the manikin surface beneath protective clothing, and the corresponding heat flux energy at specific intervals during exposure. A development of this nature eliminates the need for extensive photographic coverage of each test.

Traversing System - The complexities encountered in the design of the traversing system illustrated in Environmental Physiology Drawing No. 1, 2, and 3 of appendix D, warrant consultation with potential contractors for recommendations and development of this system. Overall design considerations include maintaining a specific velocity for passages of the manikin through the flames at 10 feet per second for 3 seconds so that proper convection currents can be simulated for the prescribed distance and time. The traversing system must be able to withstand a temperature of 1200°C for 5 minutes without deterioration of the structure or malfunction of the system. Additional considerations include a variable speed drive to adjust exposure velocity and time, and provisions to allow for more than one pass through the fire. The traversing system includes the use of synchronized doors for opening before the manikin enters and closing after it leaves the fire pit containment area, simulating a square wave pulse of energy for the fuel fire pit exposure, a crucial condition of the exposures, (reference 1).

Functional Operating System - The epoxy coating inside the fuel tanks and the rust from the galvanized piping have caused numerous delays by clogging the orifices in the fuel distribution system. Fiberglas tanks and copper or stainless piping will prevent such occurrences in the scaled-down version of the

facility. An automatic, controlled metering system for delivery of the gasoline is required with settings in one gallon increments from 0 to 30 gallons pumping at a minimum rate of one gallon per second. An electronic interlock system with automatic sequencing of controls with manual overrides are necessary for the following functions:

- 1. Opening ventilation system louvers,
- 2. filling the containment pit with water,
- 3. pressurizing the propane gas and compressed air manifolds,
- 4. pumping gasoline into the fuel fire pit,
- 5. ignition of the gasoline,

- 6. starting the recording and photographic data collection systems,
- 7. operating the doors that separate the pit from the dressing area,
- 8. operating the traversing system, and
- 9. abort with provisions for emergency execution of the fire extinguishing system.

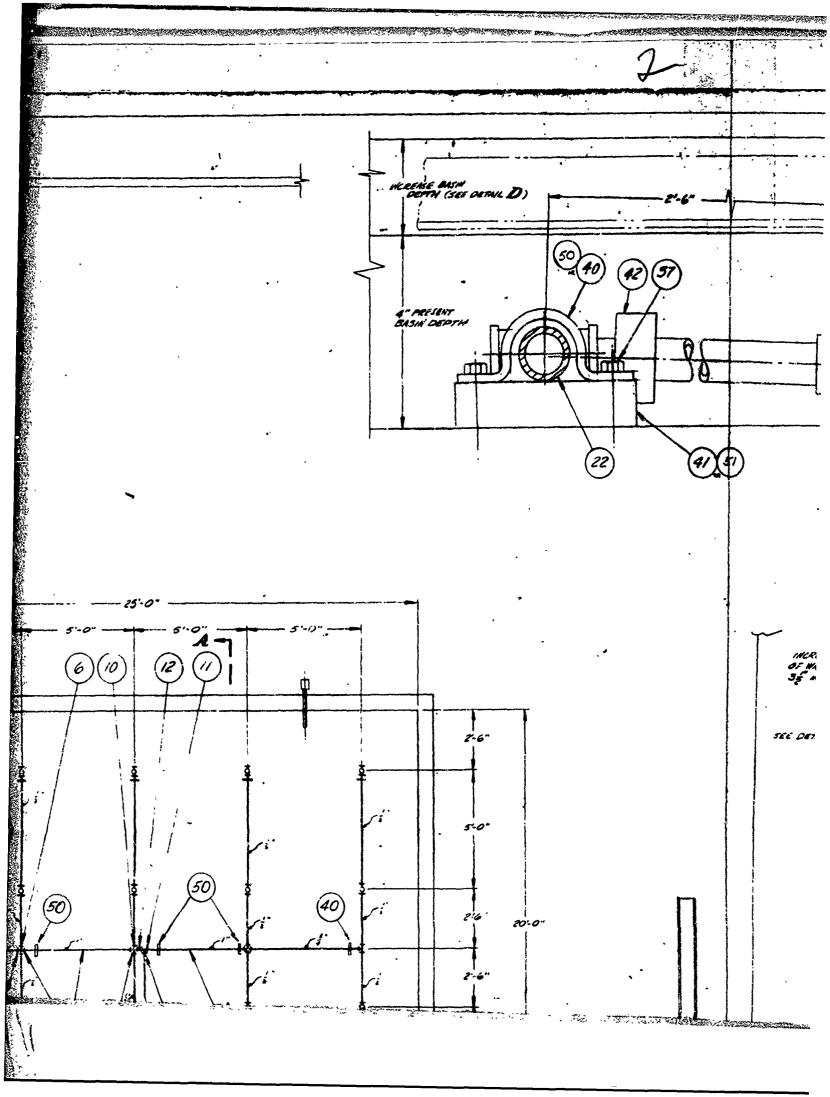
CONCLUSION

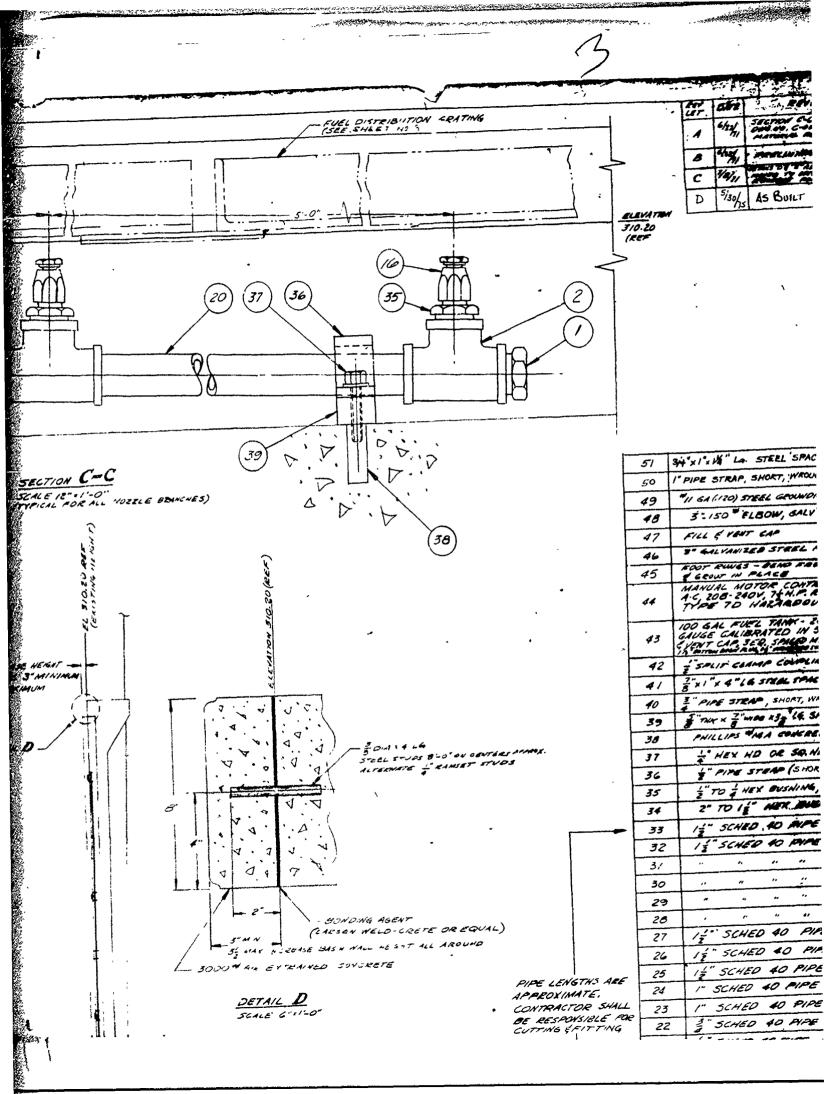
The data discussed herein, together with the drawings in the enclosures, provide the necessary basis for construction of a scaled-down version of the fuel fire facility. Each of the primary operating systems is presented independently for simplification of the total system development cycle. To this end a work breakdown structure can be formulated for the construction phase of development assigning each of the required systems to a specific descipline. This will provide tracking of the funding, scheduling, and construction performed by the individual contractors.

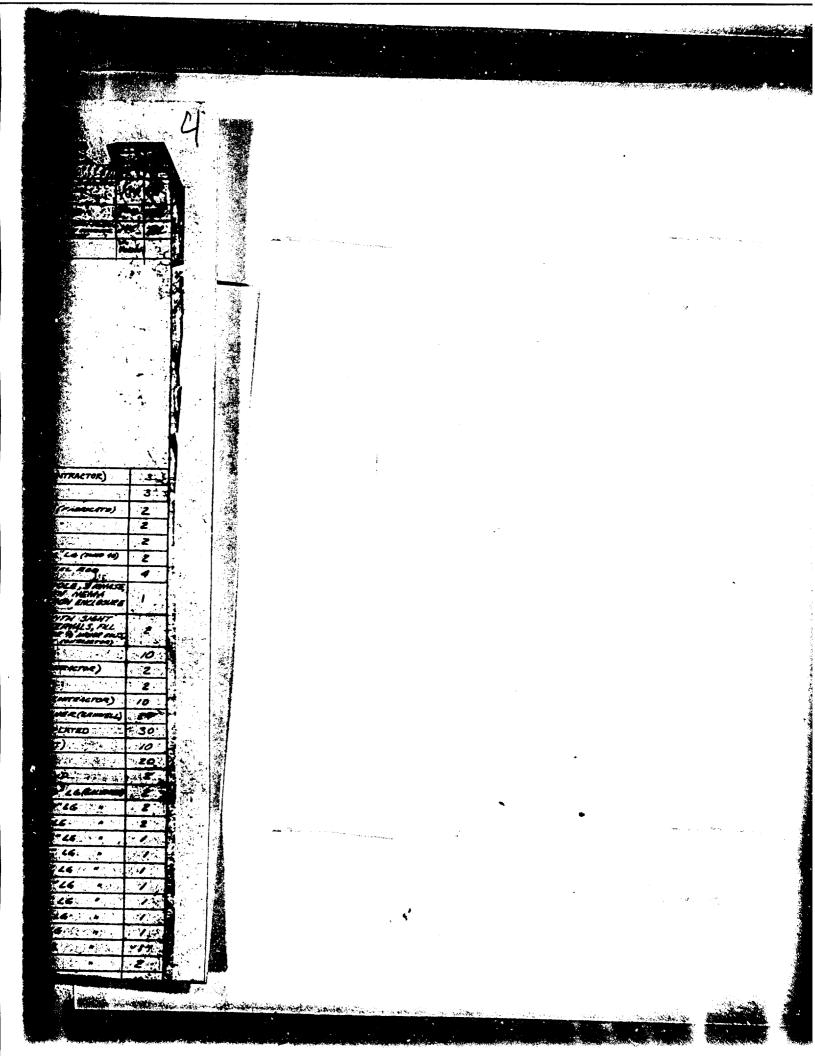
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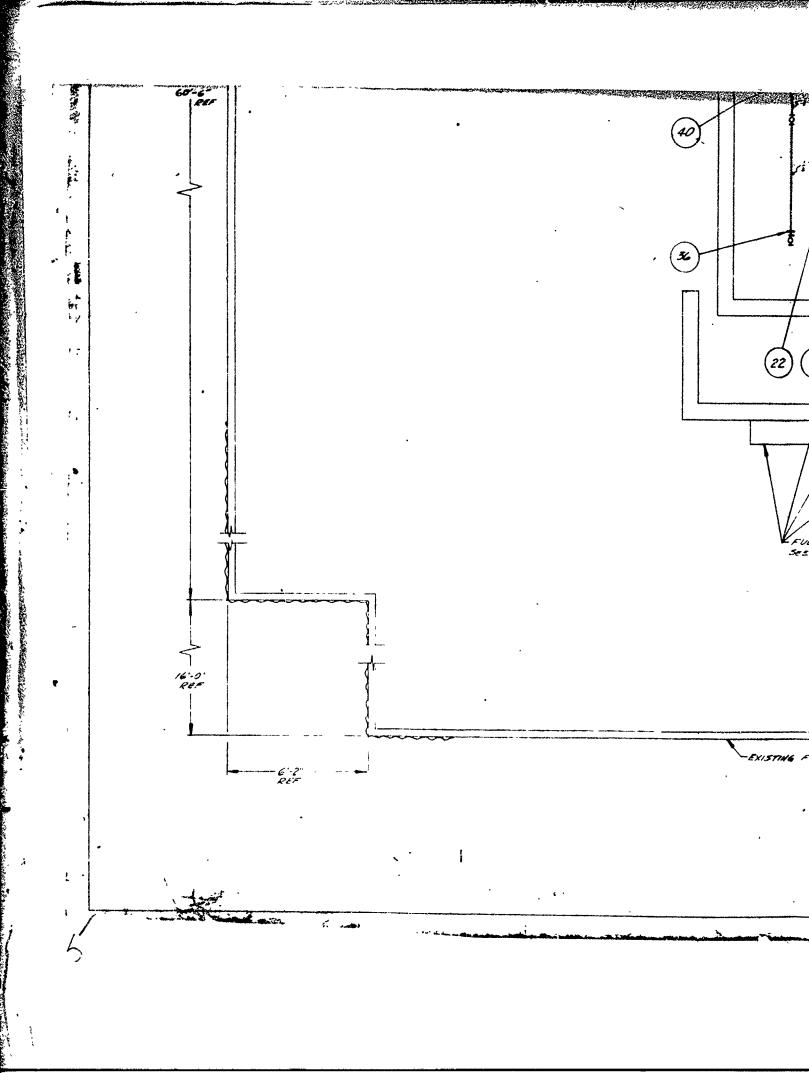
- 1. Stoll, A.M., Munroe, L.R., Chianta, M.A., Piergallini, J.R., and Zaccaria, D.E. A Facility and Method for Evaluation of Thermal Protection. Report No. NADC-75286-40 of 1 Dec 1975.
- 2. Piergallini, J.R. and Stoll, A.M., Telemetry System for Evaluation of Burn Protection in Full-Scale Fuel Fire Manikin Exposures. Aerospace Medical Association Preprint of 1976 Scientific Program 63-64, May 1976.

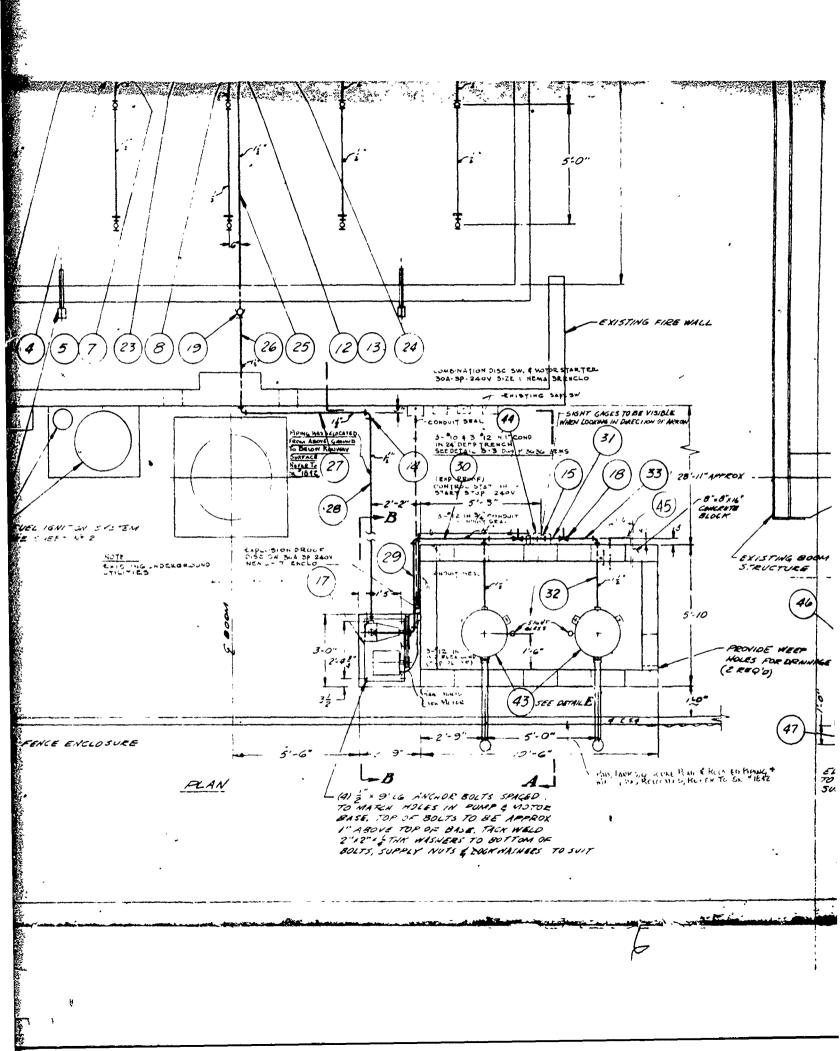
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NAVFAC DRAWINGS

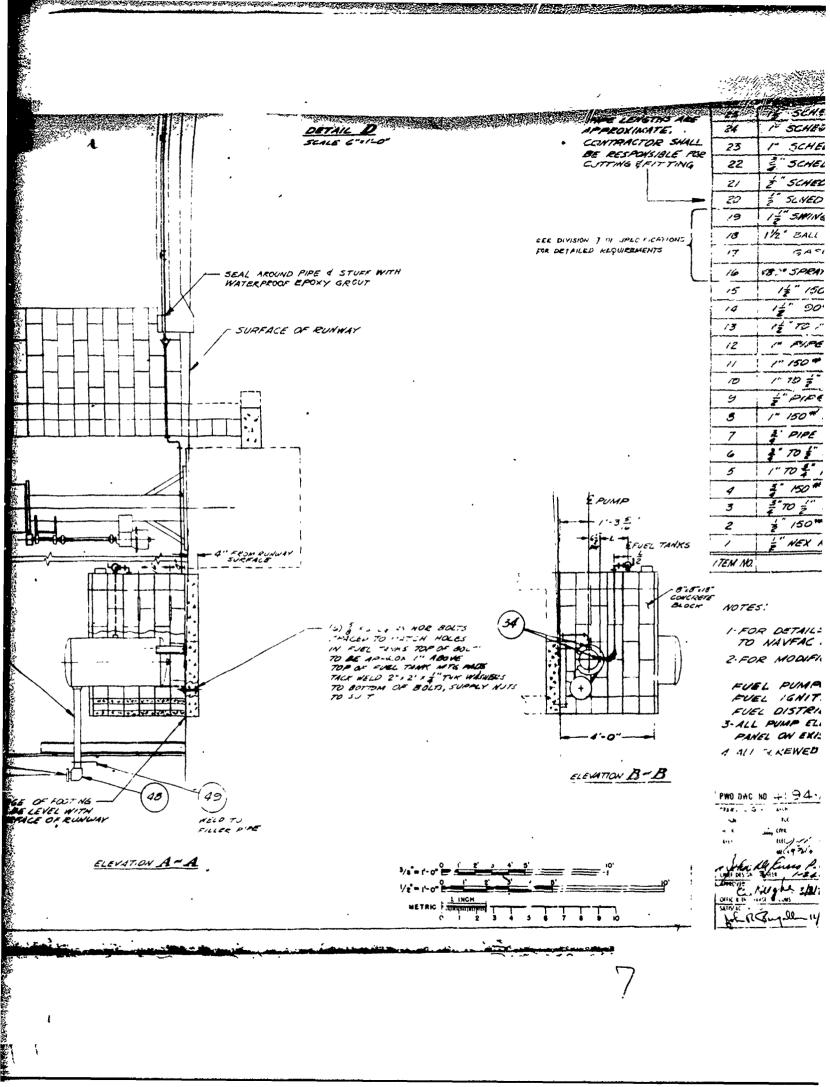












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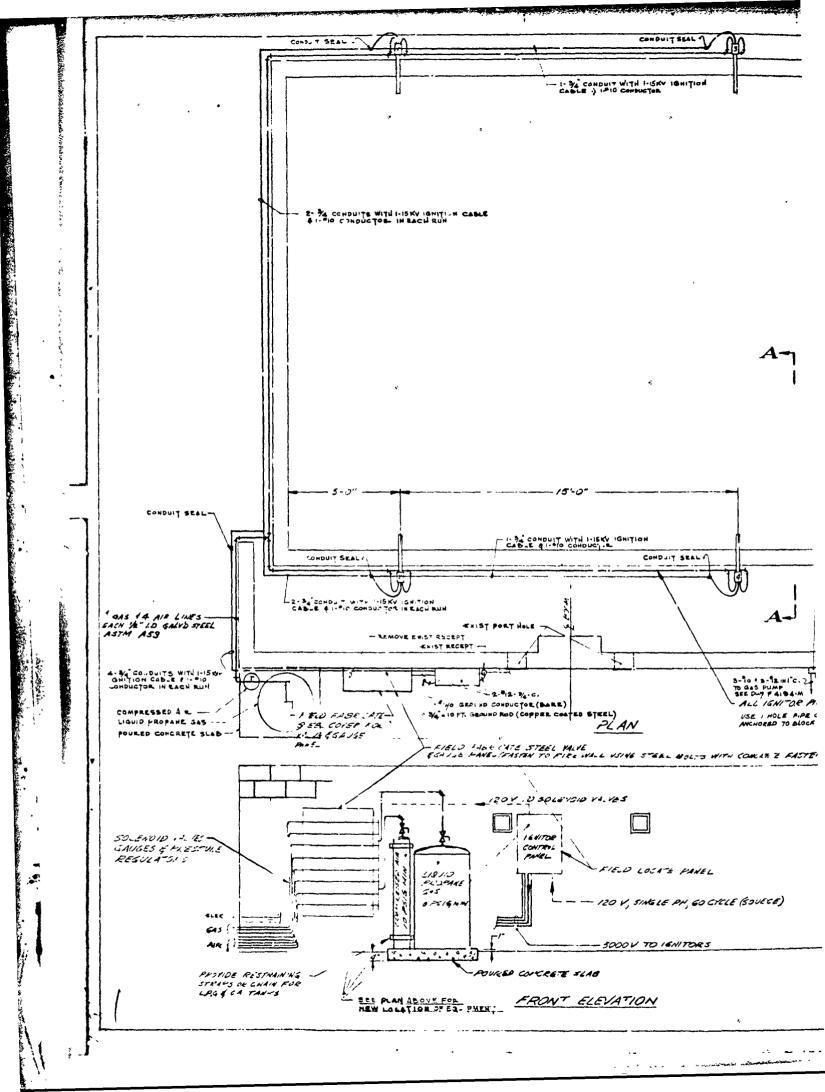
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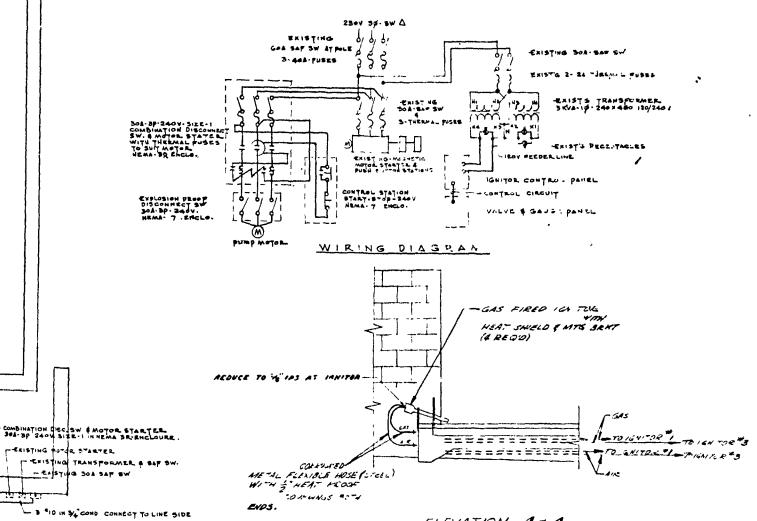
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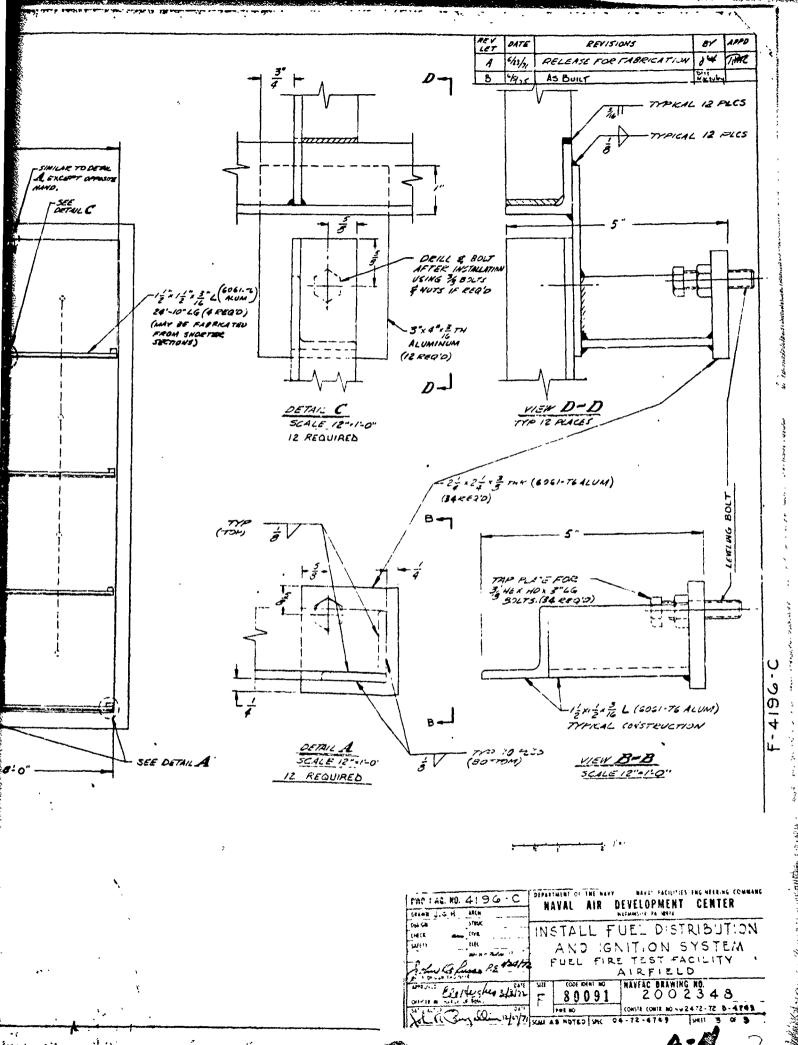
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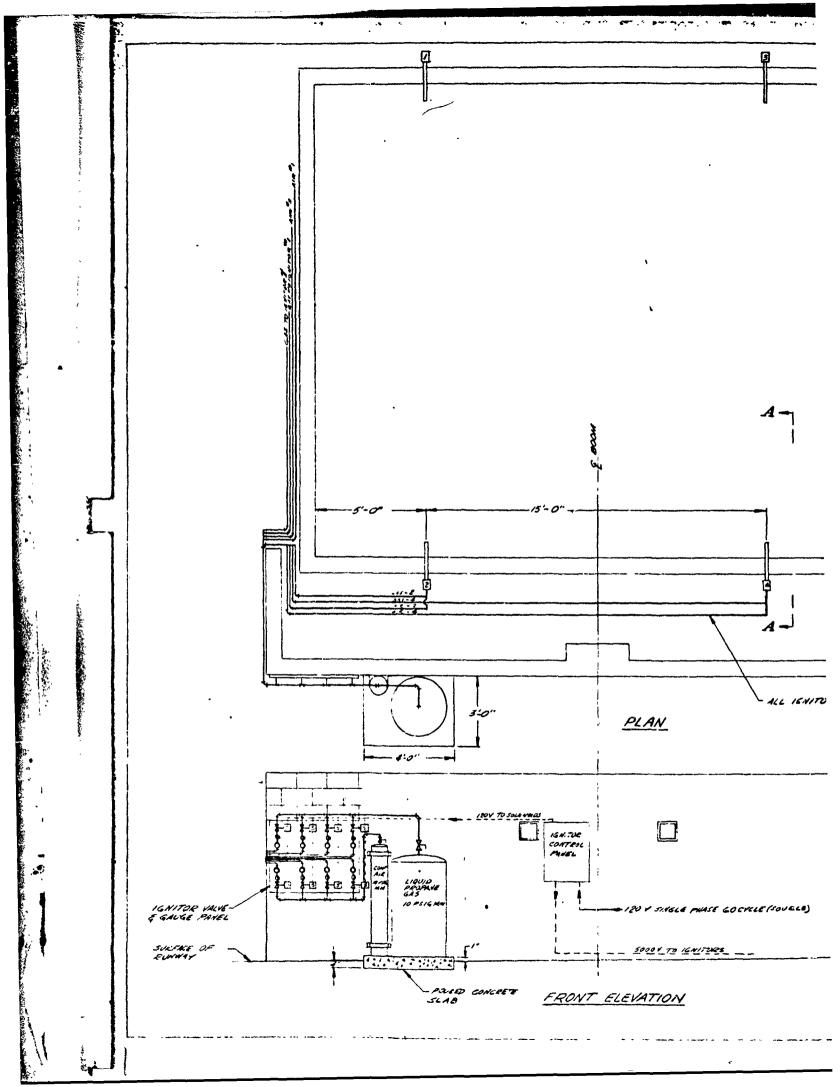
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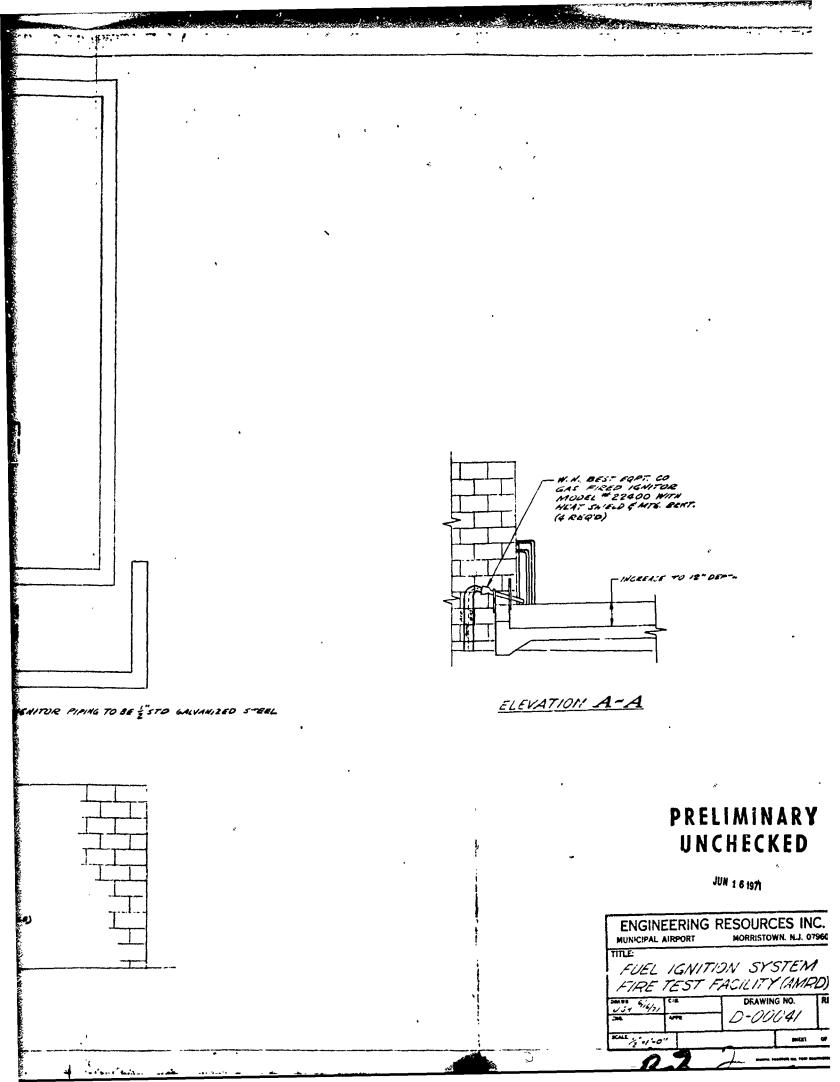
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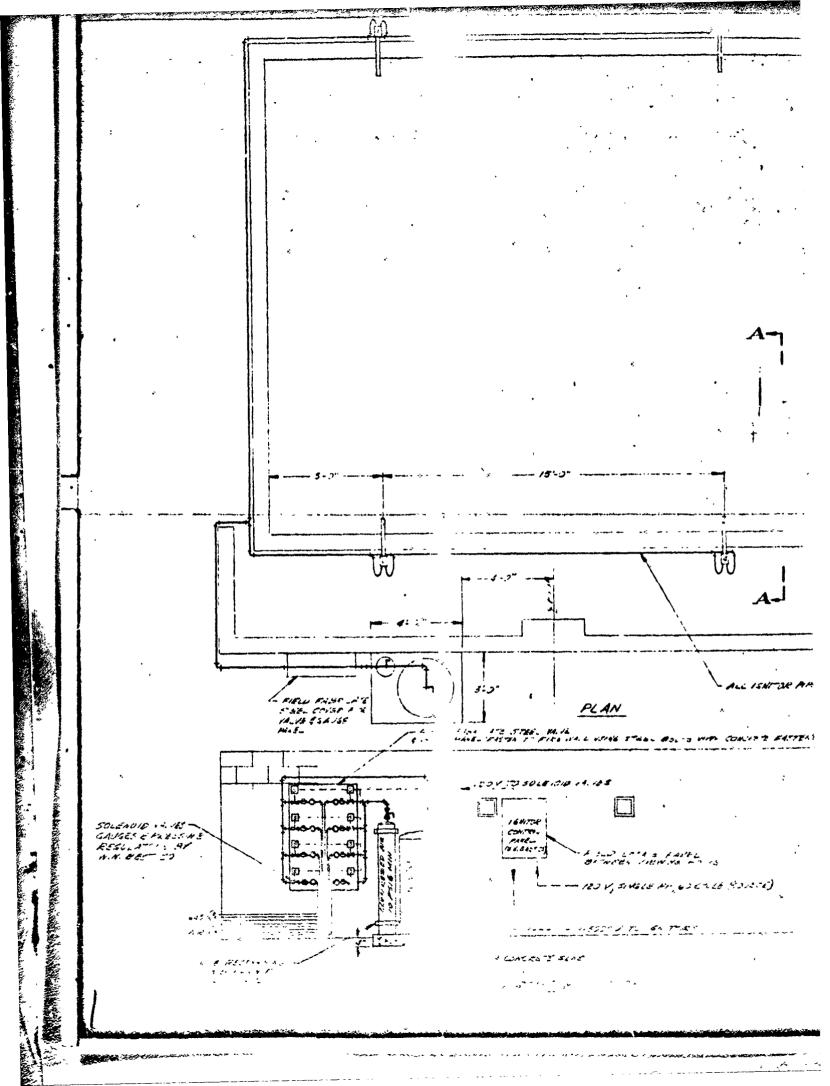


A P P E N D I X B ENGINEERING RESOURCES INC. DRAWINGS

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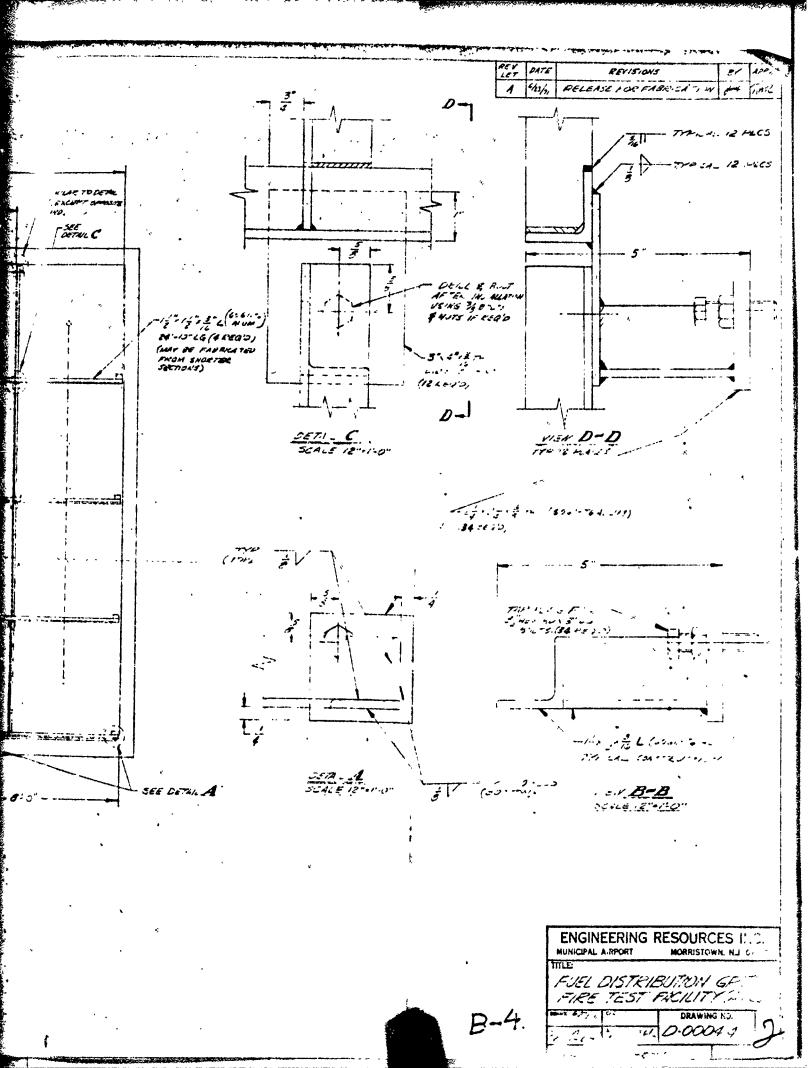
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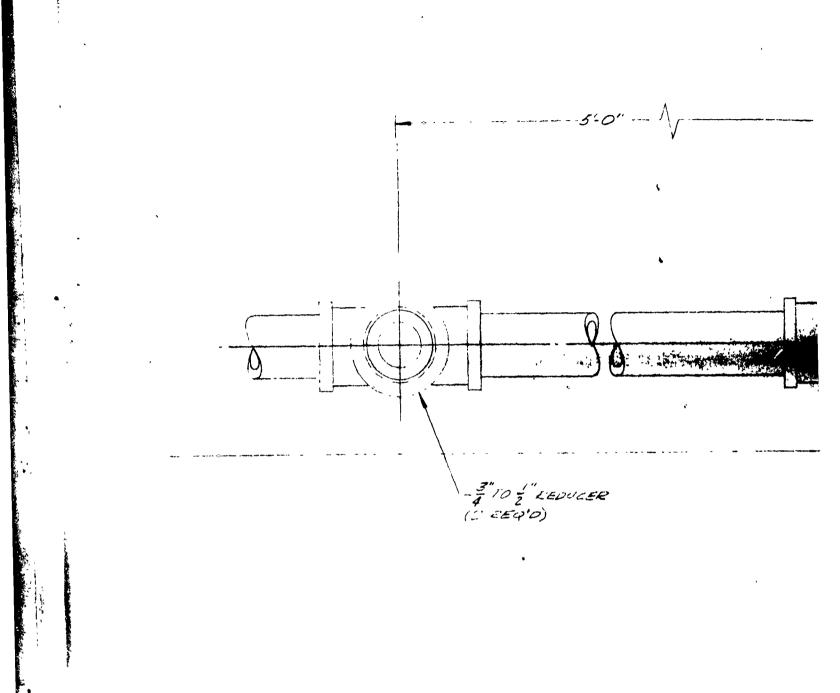
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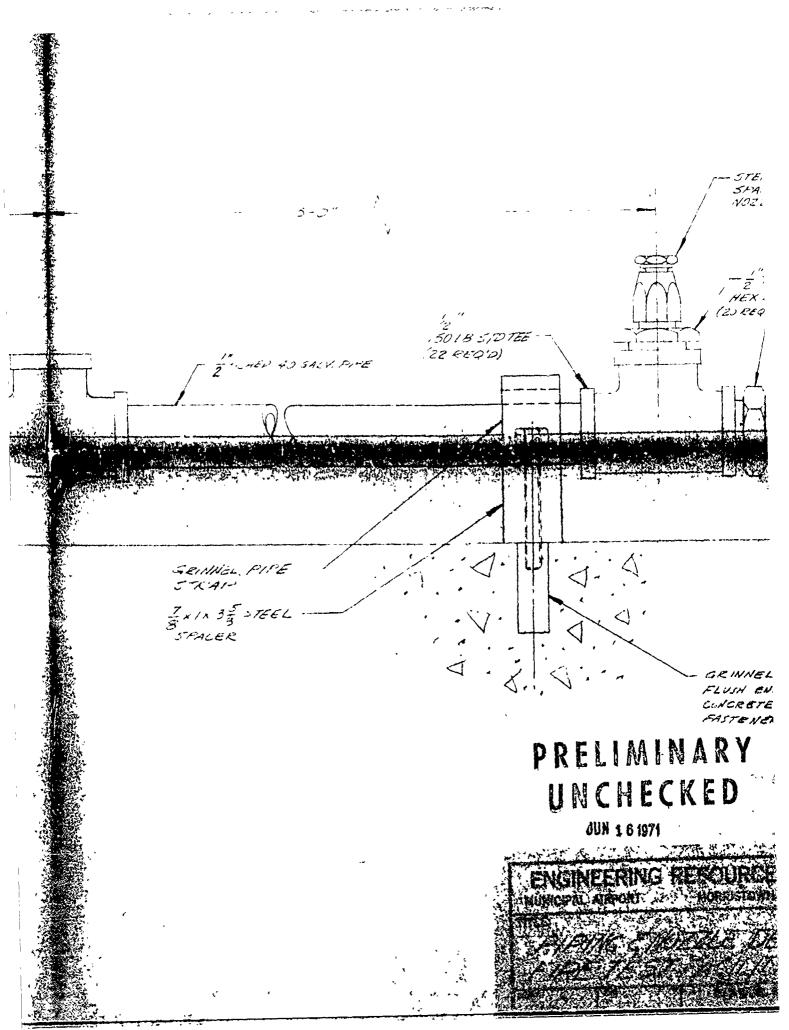
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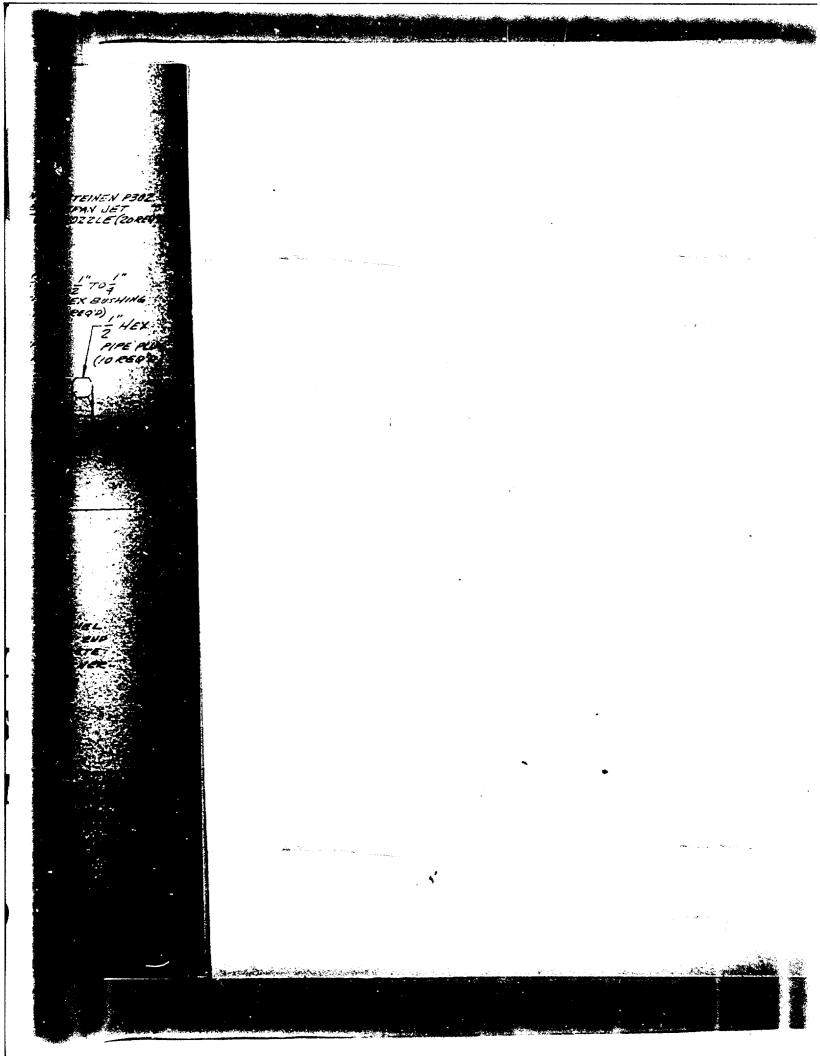
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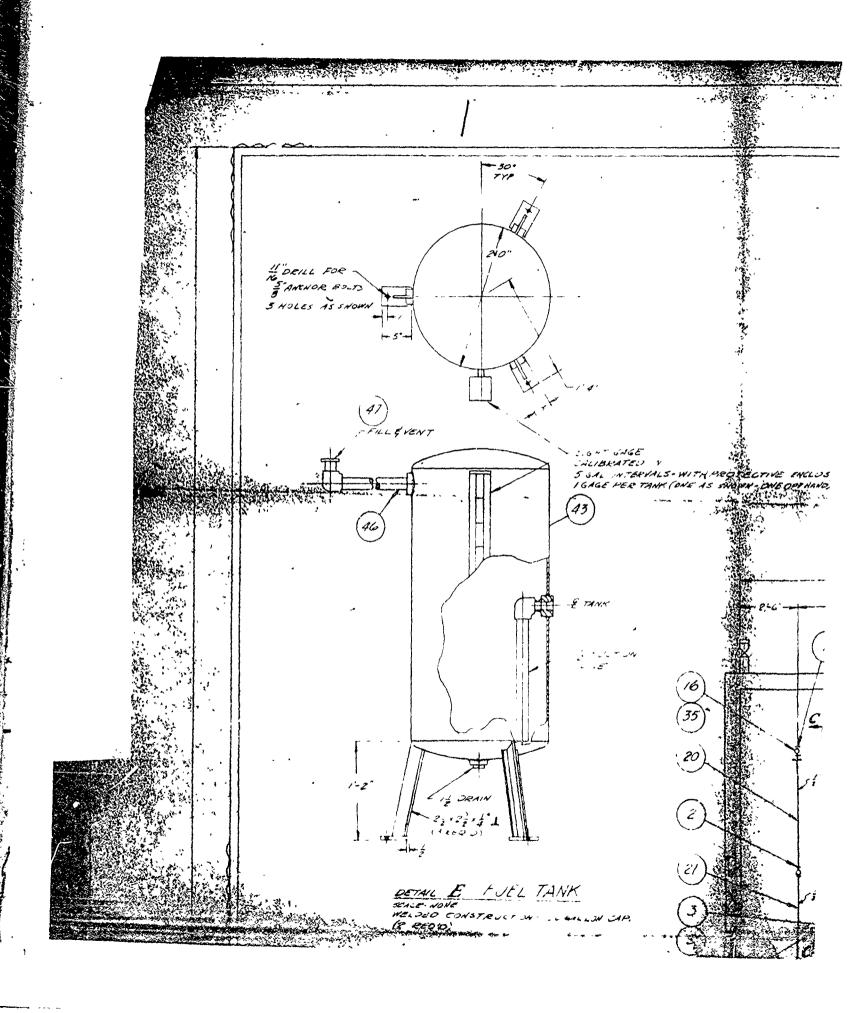
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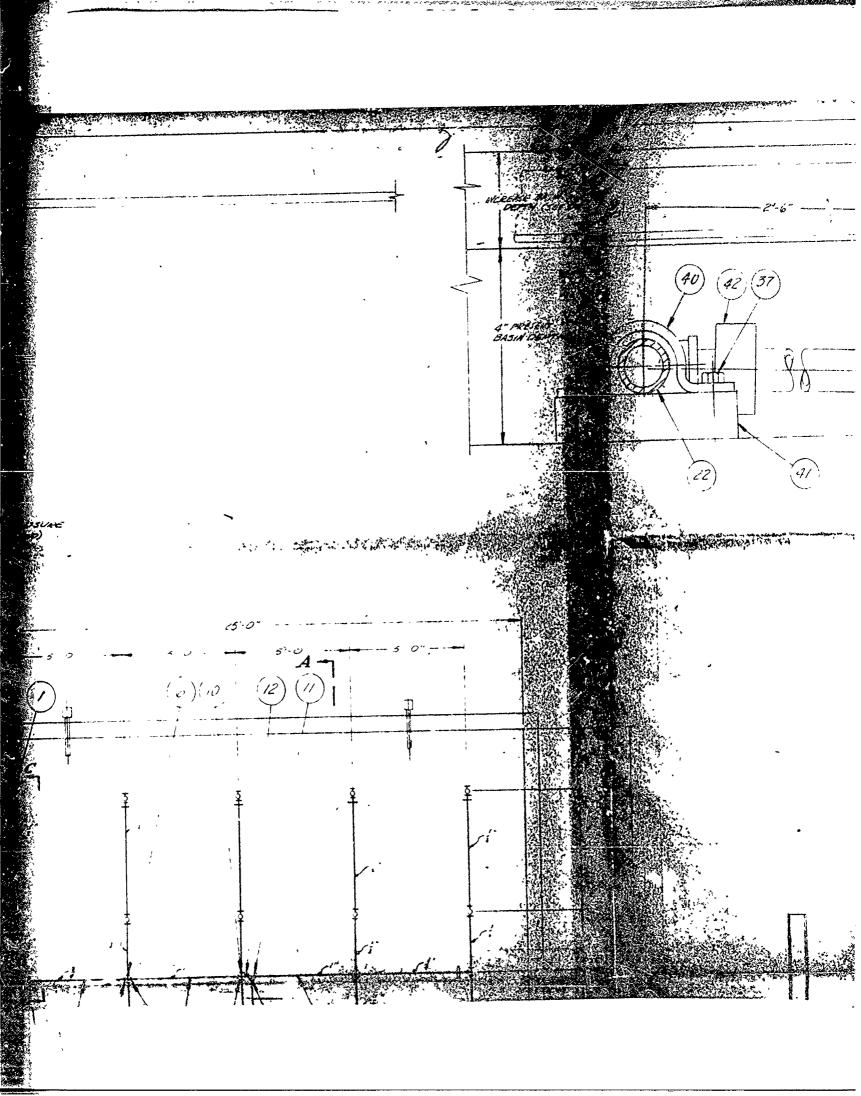


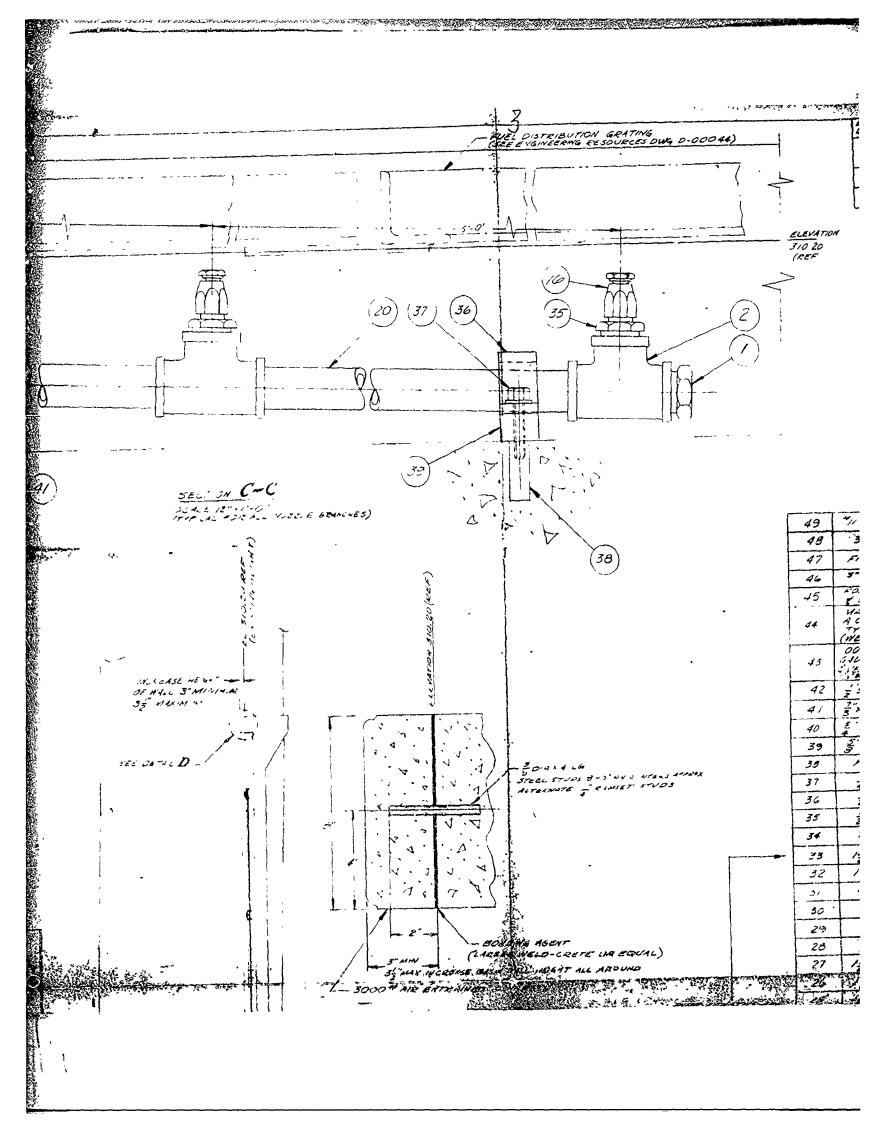










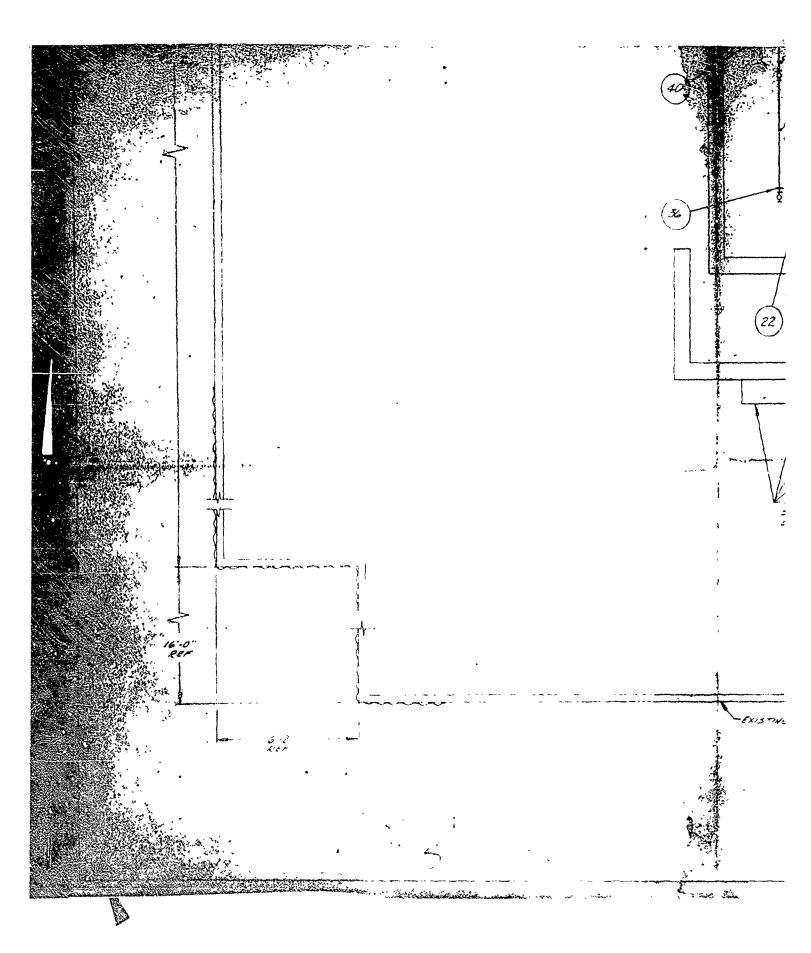


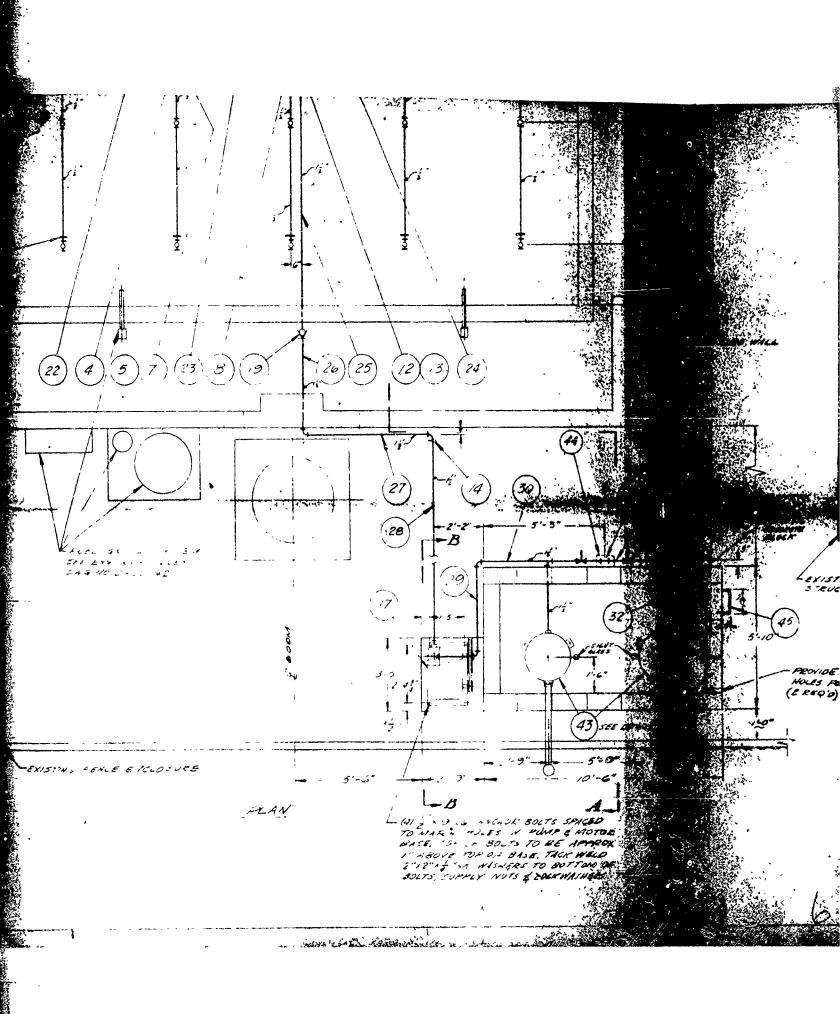
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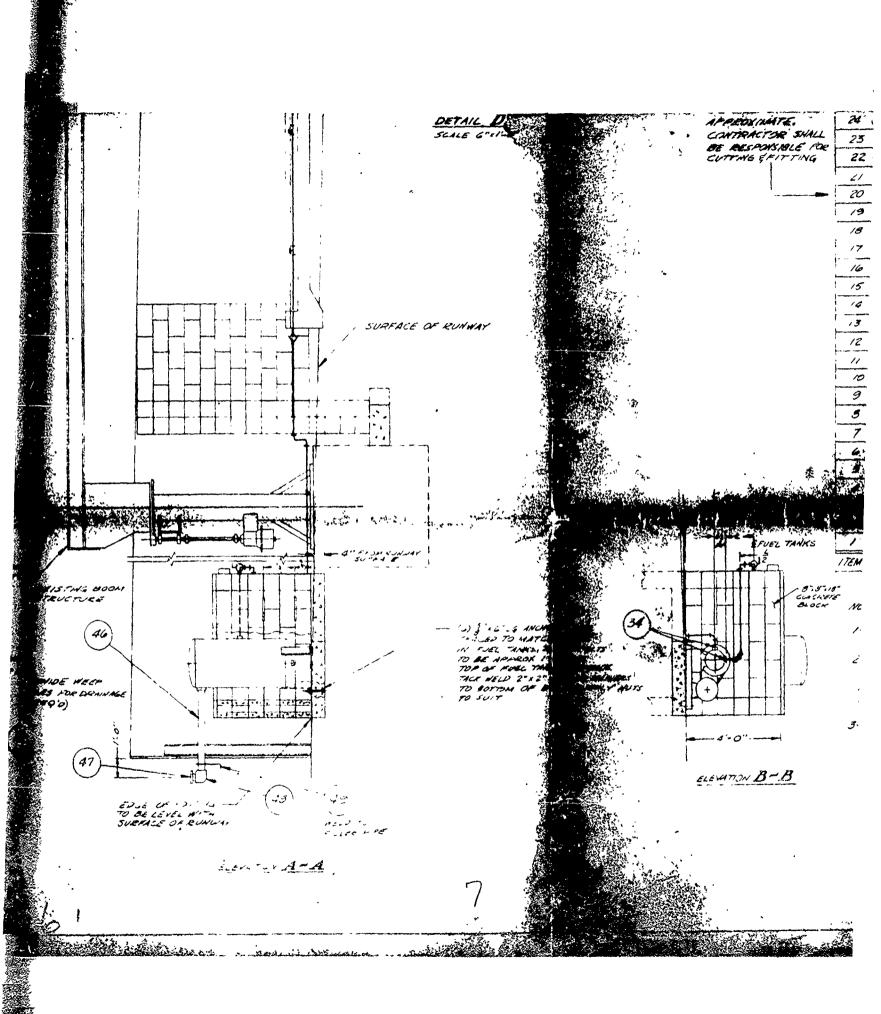
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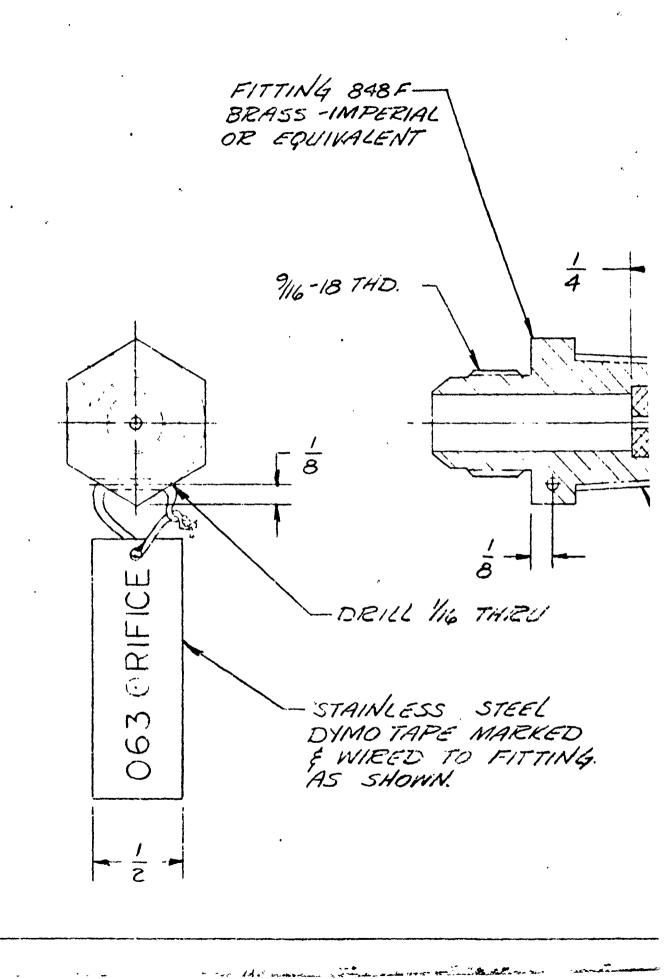
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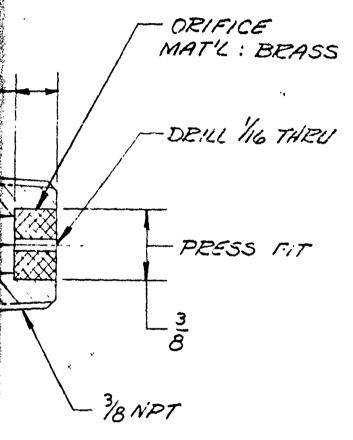
FUEL PUMPING SYSTEM J-00041 ULL SNITION SYSTEM 0-00042

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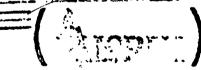




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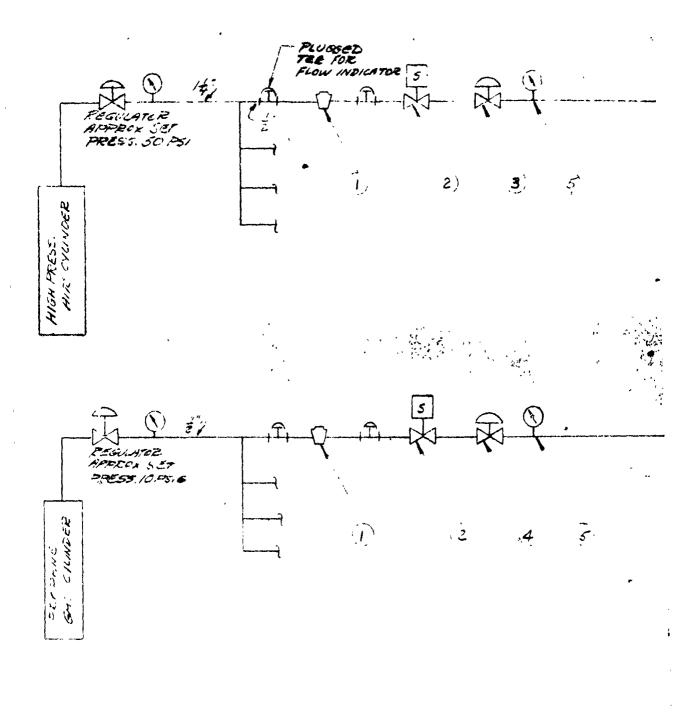


W. N. BEST COMBUSTION EQUIPMENT CO., INC.

LITTLE REWAY, NEW JERSEY

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KERNEY 12-23 71 2X DRAWING No 1/273



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17EM	GTY	NAME & DESCRIPTION
	8	IRON FLUG COLK- 2
2	8	AIR & GAS SOLEAR, D ASSC 8211694. 3
3	4	FIRE PRESCURE REGULATOR - FISHER
	-	354-1' ISEN BODY - 6 # SPRING
4	4	GAS PRESS INE KEBUCATOR F. FOR
	-	322-5: \$" - 18 rol : FSI SFRING
5		TREES GAUGA: P. M. Com. TIME
	40	16 83 2 4M . 3 - 6 10 190 " 0. 2.
	•	Sespence Meey - 1273 1783
	4	WN BEST TOWTHOR # 28400 P
		DIMENSION = 17"
8	4	HEAT SHIELD & MIG HEEV.

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· LONLY THOSE ITEMS SHOWN IN A P. P. SUPPLIED BY WIN EEST.

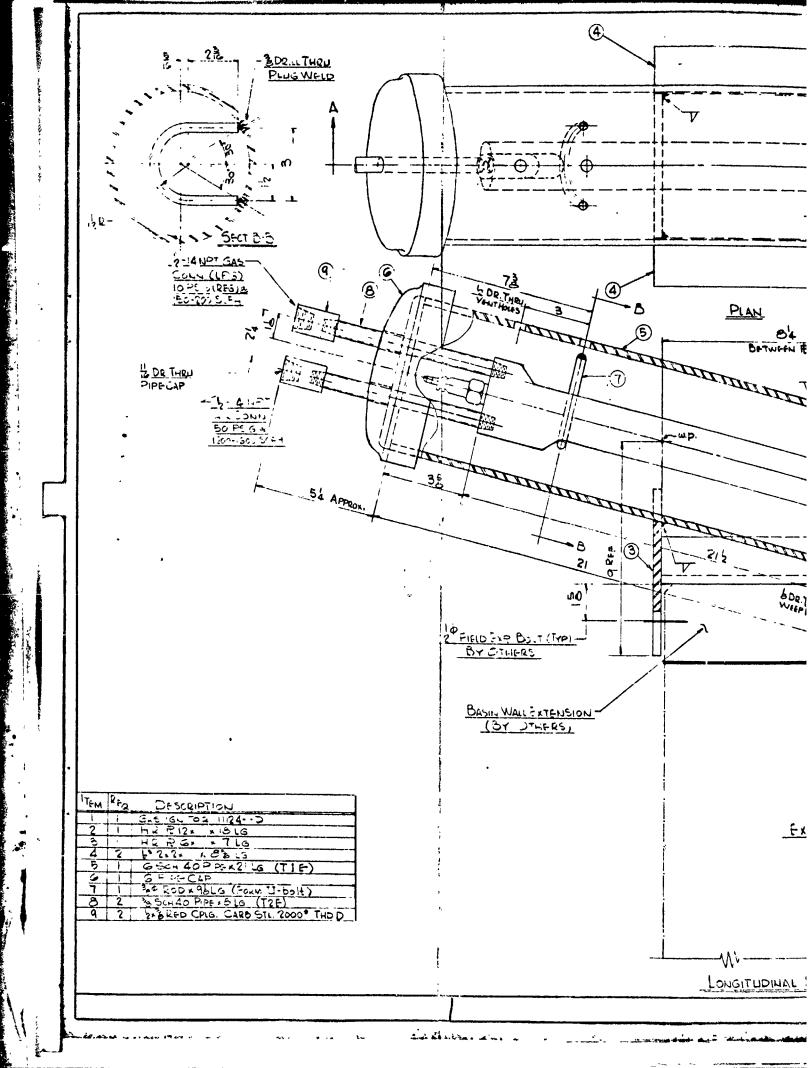
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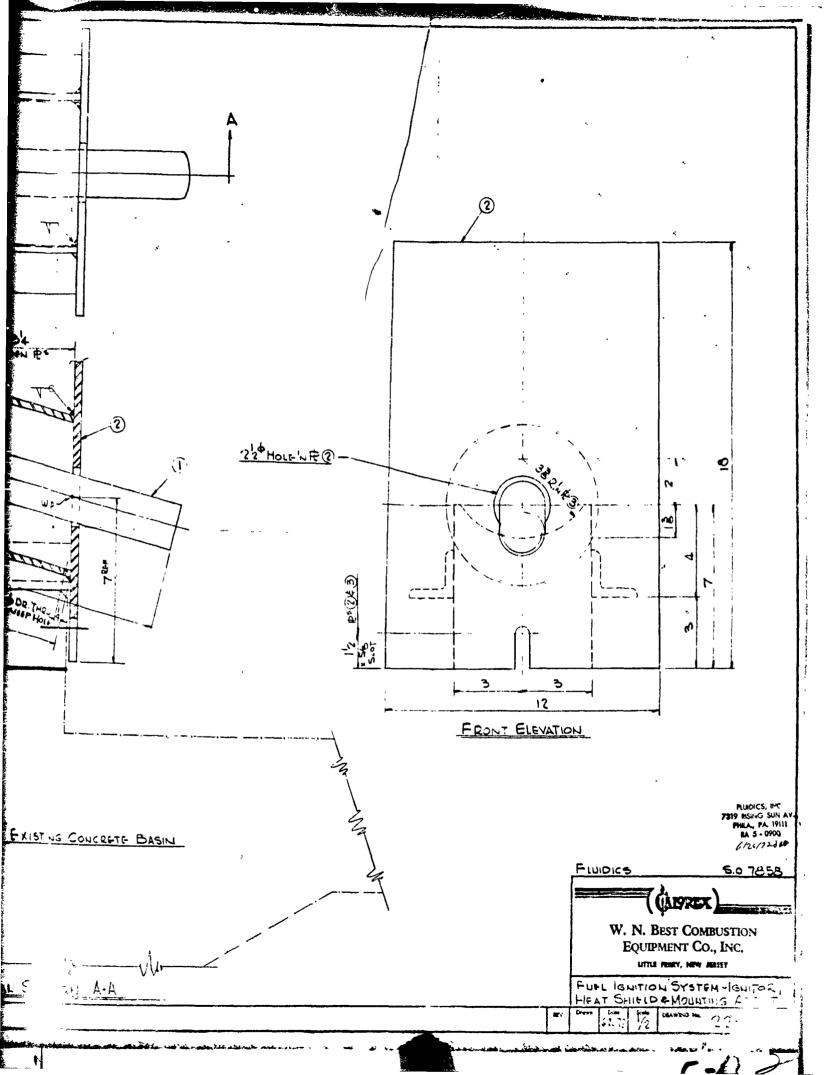
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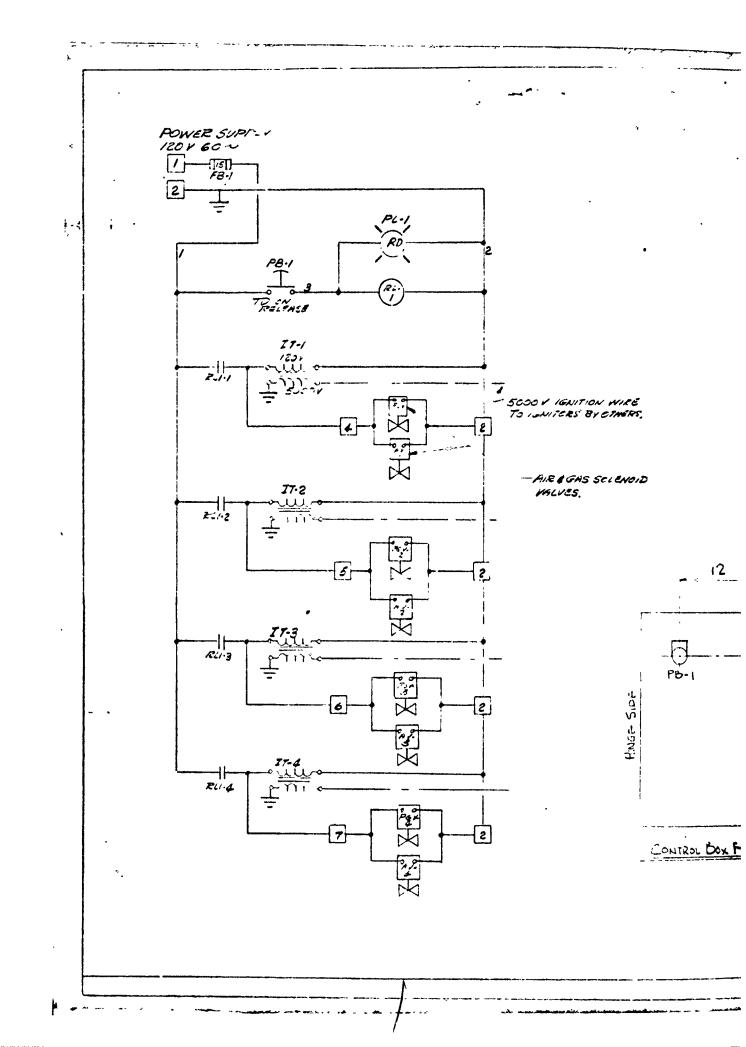
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W. N. BEST COMBUSTION EQUIPMENT Co., INC.

LITTLE FERRY, NEW JERSEY





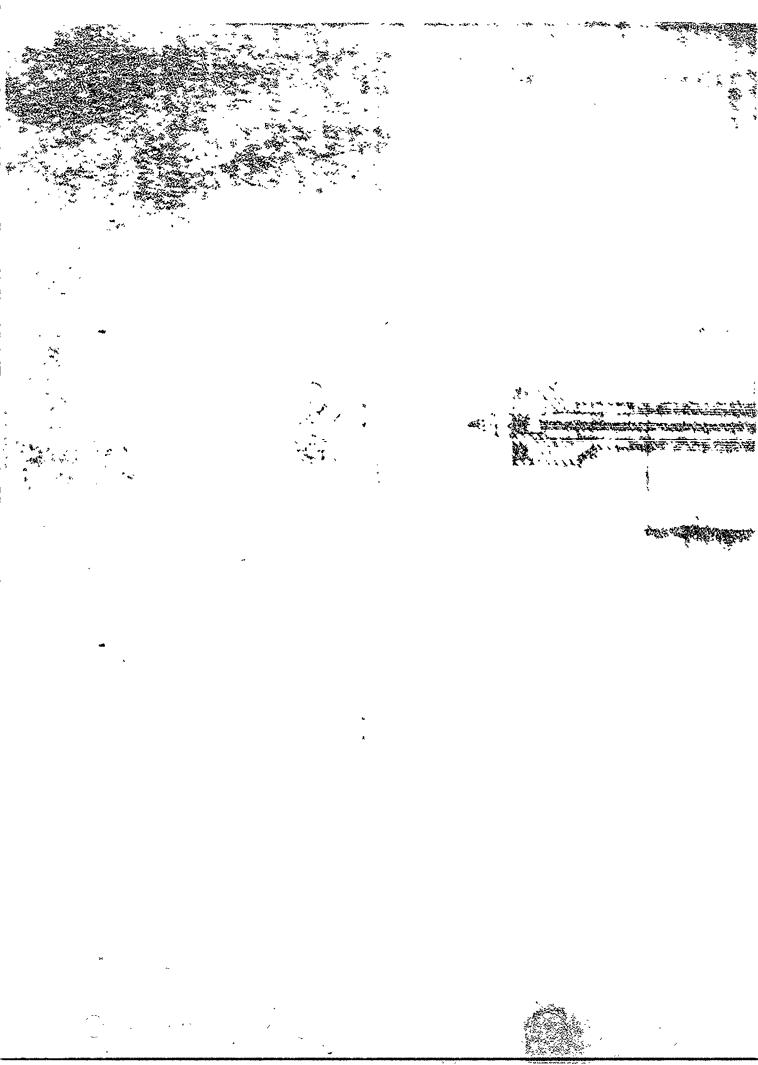


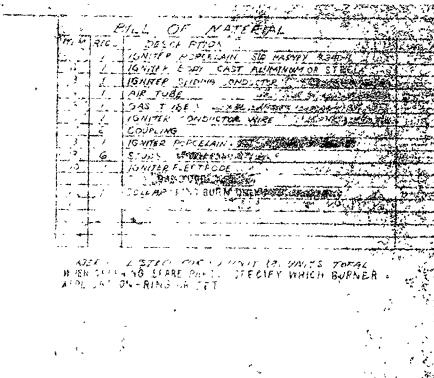
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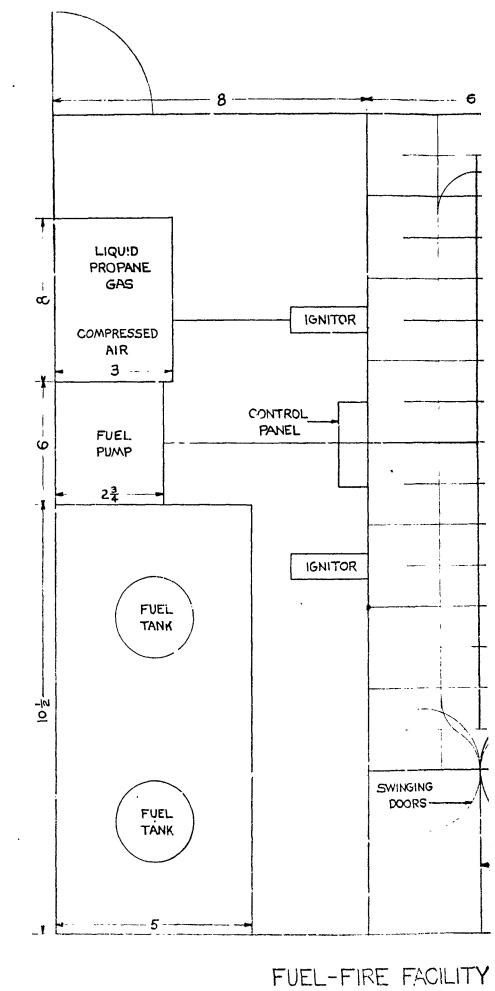
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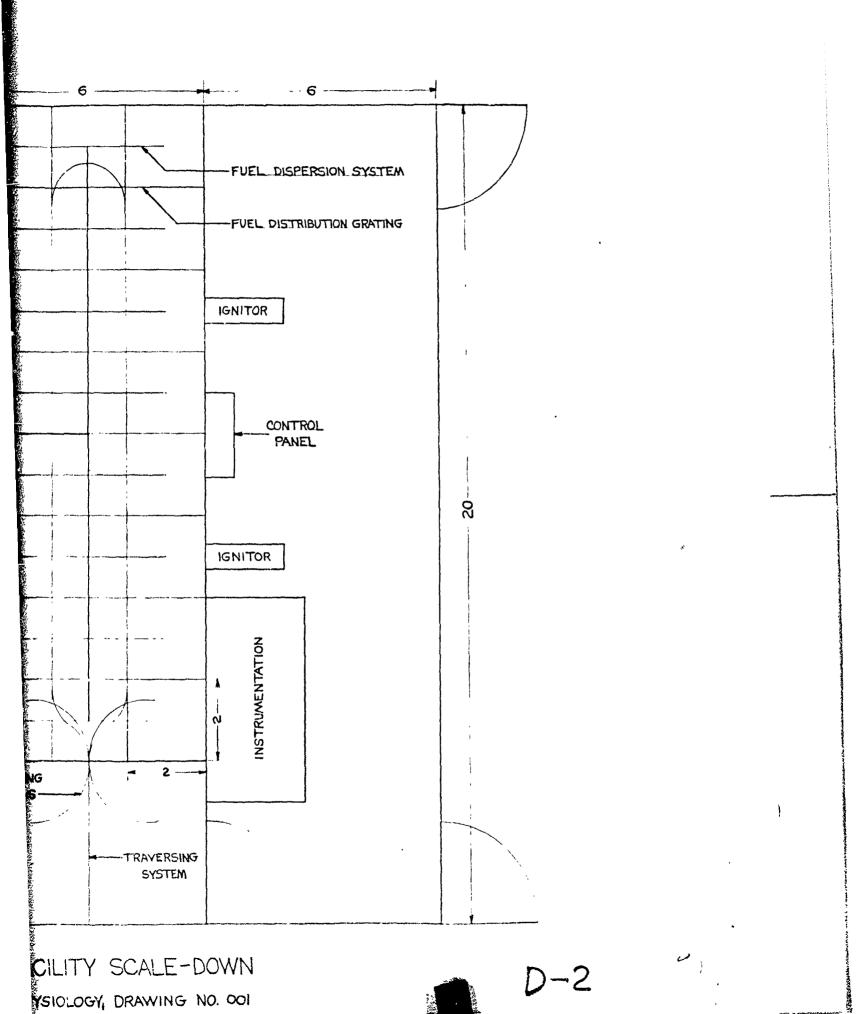
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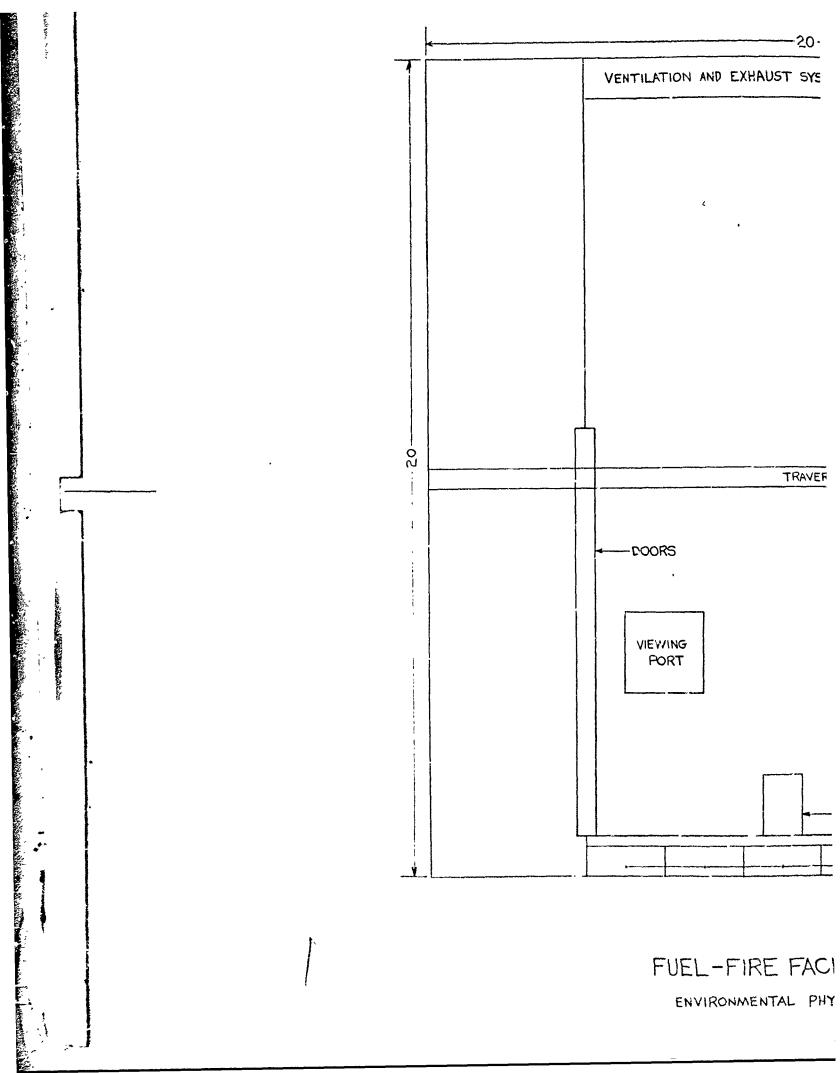
APPENDIX C

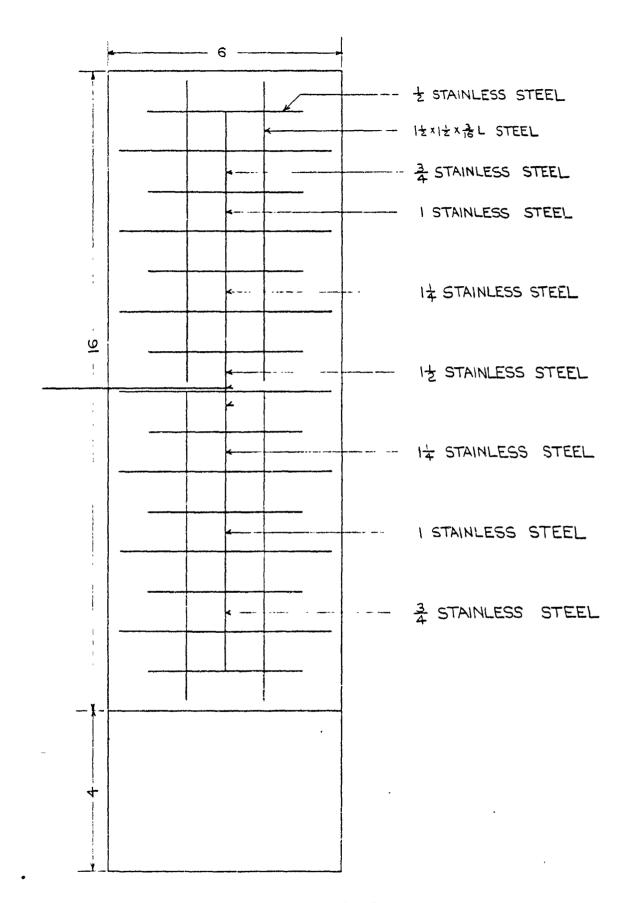
W. N. BEST COMBUSTION EQUIPMENT COMPANY, INC. DRAWINGS



FUEL-FIRE FACILITY ENVIRONMENTAL PHYSIOLOGY







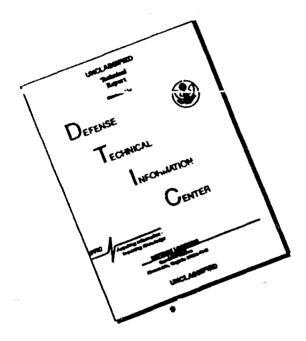
FUEL-FIRE FACILITY SCALE - DOWN ENVIRONMENTAL PHYSIOLOGY DRAWING NO. 003

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APPENDIX D

ENVIRONMENTAL PHYSIOLOGY DRAWINGS

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